

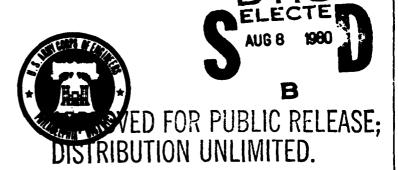
RARITAN CRANBURY BROOK, MIDDLESEX COUNT **NEW JERSEY** 

# ® BRAINERD LAKE DAM NJ 00152

9 Č

AD A 0 8

PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM



THE ARMY DEPARTMENT

> Philadelphia District Corps of Engineers Philadelphia, Pennsylvania

SECURITY CLASSIFICATION OF THIS PAG	E (When Date Entered) RIC	hard/McDermo
REPORT DOCUME		PEAD INSTRUCTIONS
1. REPORT NUMBER	• • • • • • • • • • • • • • • • • • • •	BEFORE COMPLETING FORM NO. 3. RECIPIENT'S CATALOG NUMBER
NJ00152	AD 408763	8
4. TITLE (and Subtitle)	7 3/1/10/18/5	5. TYPE OF REPORT & PERIOD COVERE
Phase I Inspection Report		- 6
National Dam Safety Programmer Brainerd Lake Dam (NJ/0/015	Doriton Diver	FINAL PED :
Middleson Country New Jorg	#BOS/N	(5)
7. AUTHOR( ) Cranbury By	rook, Middlescx	DACW61-79-C-0011
County, Ne	w Jersey.	DACWOI-19-0-0011
Phase 1 Inspect	tion Report.	
9. PERFORMING ORGANIZATION NAME	NO ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Storch Engineers / 2210 Ridgedale Ave.		
Florham Park, N.J. 07932		
11. CONTROLLING OFFICE NAME AND A NJ Department of Environme	DDRESS ental Protection	12
Division of Water Resource P.O. Box CNO29	28	Mar 1980
Trenton, NJ 08625		77
14. MONITORING AGENCY NAME & ADDR U.S. Army Engineer Distric	ESS(II different from Controlling Office to Philadelphia	ce) 18. SECURITY CLASS. (of this report)
Custom House, 2d & Chestny		Unclassified
Philadelphia, PA 19106	121 821	15a. DECLASSIFICATION/DOWNGRADING
16. DISTRIBUTION STATEMENT (of this R		
		<b>.</b>
Approved for public releas	se; distribution unlimi	itea.
17. DISTRIBUTION STATEMENT (of the at	etract entered in Block 20, If differen	nt from Report)
16. SUPPLEMENTARY NOTES		
Copies are obtainable from		formation Service,
Springfield, Virginia 221	.51.	
19. KEY WORDS (Continue on reverse elde :	il necessary and identify by block not National Dam Safet	
Embankments	Brainerd Lake Dam,	
Visual Inspection	Spillway .	•
Strucutral Analysis		
20. ABSTRACT (Continue on reverse side f		
		lgation as to the dam's adequac prescribed by the National Dam
		orescribed by the National Dam of investigation includes visua
		ruction records, and prelimina
structural and hydraulic a		
assessment of the dam's ge		
- 0-		•

DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

SECURITY CLASSIFICATION OF THIS PAGE (Then Date Entered)

SECURITY CLASSIFICATION OF THIS PAGE(Then Date Entered)	 
	1
	ļ
	I
	l
	ļ
	l
	]
	1
	Ì
	- 1
	ļ
	}
	1
	j



# DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT, CORPS OF ENGINEERS CUSTOM HOUSE—2 D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106

ACCESSION	1 for		
MTIS	Wille Section		
<b>90</b> 0	Buff Section E		
BINAMINOUS	NCSD [2]		
<b>ANS</b> TIFICAT	rich		
BY BESTROUTHOR/AYAILABILITY CODES Bist. AVAIL and or bregial			
Sible A	TAIL BILL DE STECHE		
A			

Honorable Brendan T. Byrne Governor of New Jersey Trenton, New Jersey 08621

04 AUG 1980

#### Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Brainerd Lake Dam in Middlesex County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Brainerd Laba Nam, initially listed as a "high" hazard potential structure, but reduced to a "significant" inazard potential structure as a result of this inspection, is judged to be in fair overall condition. The dam's spillway is considered inadequate because a flow equivalent to 17 percent of the 100-year flood would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. The adequacy of the spillway should be determined using more precise and sophisticated methods and procedures by a qualified, professional consultant, engaged by the owner, within six months from the date of approval of this report. Within three months of the consultant's findings, remedial measures to ensure spillway adequacy should be initiated.
- b. Within six months from the date of approval of this report the following remedial actions should be initiated:
- (1) With the lake drawn down, the masonry wall on the upstream side of dam should be thoroughly inspected and repaired.
- (2) The spillway structure and discharge culvert should be thoroughly inspected and repaired with the lake drawn down. Special attention should be given to the possibility of leakage in the spillway structure around the outlet works and to the crack at the downstream end of the discharge culvert.

NAPEN-N Honorable Brendan T. Byrne

- (3) Trees on the embankment should be removed.
- (4) The partially rotted planks on the walkway should be replaced.
- d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam within one year from the date of approval of this report.
- e. The owner should develop an emergency action plan together with an effective warning system outlining actions to be taken by the operator to minimize downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Patton of the Fifteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

1 Incl
As stated

JAMES G. TON

Colonel, Corps of Engineers

District Engineer

Copies furnished: Mr. Dirk C. Hofman, P.E., Deputy Director Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief Bureau of Flood Plain Regulation Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

#### BRAINERD LAKE DAM (NJ00152)

#### CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 12 November 1979 by Storch Engineers under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Brainerd Lake Dam, initially listed as a Phigh hazard potential structure. but reduced to a \*significant\* hazard potential structure as a result of this inspection, is judged to be in fair overall condition. The dam's spillway is considered inadequate because a flow equivalent to 17 percent of the 100-year flood would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. The adequacy of the spillway should be determined using more precise and sophisticated methods and procedures by a qualified, professional consultant, engaged by the owner, within six months from the date of approval of this report. Within three months of the consultant's findings, remedial measures to ensure spillway adequacy should be initiated.
- b. Within six months from the date of approval of this report the following remedial actions should be initiated:
- (1) With the lake drawn down, the masonry wall on the upstream side of dam should be thoroughly inspected and repaired.
- The spillway structure and discharge culvert should be thoroughly inspected and repaired with the lake drawn down. attention should be given to the possibility of leakage in the spillway structure around the outlet works and to the crack at the downstream end of the discharge culvert.
  - (3) Trees on the embankment should be removed.
  - The partially rotted planks on the walkway should be replaced.
- d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam within one year from the date of approval of this report.
- The owner should develop an emergency action plan together with an effective warning system outlining actions to be taken by the operator to minimize downstream effects of an emergency at the dam within six months from the date of approval of this report.

APPROVED: JAMES G. TON

Colonel, Corps of Engineers

District Engineer

DATE: 9 July 1950

# PHASE I REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Brainerd Lake Dam, N.J.00152

State Located:

New Jersey

County Located:

Middlesex

Drainage Basin:

Raritan River

Stream:

Cranbury Brook

Date of Inspection:

November 12, 1979

# Assessment of General Condition of Dam

Based on visual inspection, past operational performance and Phase I engineering analysis, Brainerd Lake Dam is assessed as being in fair overall condition.

Based on investigations of the downstream flood plain made in connection with this report, it is recommended that the hazard potential classification be downgraded from high to significant hazard.

Hydraulic and hydrologic analyses indicate that the spillway is inadequate. Discharge capacity of the spillway is not sufficient to pass the designated spillway design flood (100-year storm) without an overtopping of the dam. The spillway is capable of passing approximately 16 percent of the spillway design flood. Therefore, the owner should engage a professional engineer experienced in the design and construction of dams in the near future to perform more accurate hydraulic and hydrologic analyses. Based on the findings of the analyses, the need for and type of remedial measures should be determined and then implemented.

The owner should, in the near future, develop an emergency action plan together with an effective warning system outlining actions to be taken by the operator to minimize downstream effects of an emergency at the dam.

In addition, it is recommended that the following remedial measures be implemented by the owner in the near future.

- With the lake drawn down, the masonry wall on the upstream 1) side of dam should be thoroughly inspected and repaired.
- 2) The spillway structure and discharge culvert should be thoroughly inspected and repaired with the lake drawn down. Special attention should be given to the possibility of leakage in the spillway structure around the outlet works. Also, special attention should be given to the crack at the downstream end of the discharge culvert.
- 3) Trees on the embankment should be removed.
- 4) The partially rotted planks on the walkway should be replaced.

In the near future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to insure the safety of the dam.

John E. Gribbin, P.E.



OVERVIEW - BRAINERD LAKE DAM

29 NOVEMBER 1979

# TABLE OF CONTENTS

	<u>Page</u>
ASSESSMENT OF GENERAL CONDITION OF DAM	í
OVERVIEW PHOTO	iii
TABLE OF CONTENTS	iv
PREFACE	<b>v</b> i
SECTION 1 - PROJECT INFORMATION .	1
1.1 General	
1.2 Description of Project	
1.3 Pertinent Data	
SECTION 2 - ENGINEERING DATA	8
2.1 Design	
2.2 Construction	
2.3 Operation	
2.4 Evaluation	
SECTION 3 - VISUAL INSPECTION	9
3.1 Findings	
SECTION 4 - OPERATIONAL PROCEDURES	12
4.1 Procedures	
4.2 Maintenance of Dam	
4.3 Maintenance of Operating Facilities	
4.4 Description of Warning System	
4.5 Evaluation	

# TABLE OF CONTENTS (cont.)

		Page
SECTION	5 - HYDRAULIC/HYDROLOGIC	14
5.1	Evaluation of Features	
SECTION	6 - STRUCTURAL STABILITY	16
6.1	Evaluation of Structural Stability	
SECTION	7 - ASSESSMENT AND RECOMMENDATIONS	18
7.1	Dam Assessment	
7.2	Recommendations	
PLATES		
1	KEY MAP	
2	VICINITY MAP	
3	SOIL MAP	
4	GENERAL PLAN	
5	SPILLWAY SECTION	
6	DAM SECTION	
7	PHOTO LOCATION PLAN	
APPENDI	CES	
1	Check List - Visual Inspection	
	Check List - Engineering Data	
2	Photographs	
3	Engineering Data	
4	Hydraulic/Hydrologic Computations	
5	Bibliography	

•

# **PREFACE**

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 30214. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that the unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

# PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

BRAINERD LAKE DAM, I.D. NJ00152

SECTION 1: PROJECT INFORMATION

# 1.1 General

# a. Authority

Public Law 92-367, August 8, 1972 authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The Division of Water Resources of the New Jersey Department of Environmental Protection (NJDEP) in cooperation with the Philadelphia District of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the State of New Jersey. Storch Engineers has been retained by the NJDEP to inspect and report on a selected group of these dams. The NJDEP is under agreement with the Philadelphia District of the Corps of Engineers.

#### b. Purpose of Inspection

The visual inspection of Brainerd Lake Dam was made on November 12, 1979. The purpose of the inspections was to make a general assessment of the structural integrity and operational adequacy of the dam structure and its appurtenances.

# 1.2 Description of Project

#### a. Description of Dam and Appurtenances

Brainerd Lake Dam consists of an earthfill, roadway embankment, with a concrete horseshoe, overflow spillway. Water which passes over the spillway discharges through the dam via a stone and brick arch culvert.

The overall length of the dam, which is oriented north/south, is 382 feet. The embankment has a top width of approximately 40 feet. A public paved road in generally good condition is located on the crest. The downstream face of the embankment is grass covered and has a uniform slope of 3 horizontal to 1 vertical. The upstream face of the dam consists of a vertical masonry wall with a concrete cap. The crest elevation of the dam is 90.1 National Geodetic Vertical Datum (N.G.V.D.) and the elevation of the stream bed downstream from the dam is 77.6. The height of the dam is 12.5 feet. The concrete, horseshoe shaped spillway has verticle faces both upstream and downstream, with a crest breadth of 1.2 feet and overall length of 34 feet. The spillway crest elevation is 87.2 (N.G.V.D.).

The outlet works operating mechanism is located at the center of the spillway crest and obstructs 2 feet of its length. The outlet works consists of a 42-inch diameter opening in the upstream end of the spillway structure controlled by a lift gate fitted to the upstream side of the wall.

A timber walkway with steel pipe railings spans the spillway stilling basin and connects the outlet control with the upstream face of dam.

#### b. Location

Brainerd Lake Dam is located in the Township of Cranbury, Middlesex County, New Jersey. The dam impounds Brainerd Lake, used primarily for recreational purposes. Discharge from the spillway of the dam flows into Cranbury Brook. Access to the dam is provided by a county road (Route 535), known as Georges Road or Main Street, which traverses the dam crest.

# c. Size and Hazard Classification

Size and Hazard Classification criteria presented in "Recommended Guidelines for Safety Inspection of Dams," published by the U.S. Army Corps of Engineers are as follows:

Impoundment

# SIZE CLASSIFICATION

	<u> </u>			
	Storage (Ac-ft)		Height (Ft.)	
Small	<1000 and	50	<40 and≥ 25	
Intermediate	≥1000 and	50,000	≥40 and < 100	
Large	≥50,000		≥ 100	

# HAZARD POTENTIAL CLASSIFICATION

Category	Loss of Life	Economic Loss
	(Extent of Development)	(Extent of Development)
Low	None expected (no per-	Minimal (Undeveloped to
	manent structures for	to occasional structures
	human habitation	or agriculture)
Significant	Few (No urban develop-	Appreciable (Notable
•	ments and no more than	agriculture, industry
	a small number of	or structures)
	inhabitable structures	
High	More than a small	Excessive (Extensive
	number	community, industry or
		agriculture)

The following data relating to size and downstream hazard for Brainerd Lake Dam have been obtained for this Phase I assessment:

Storage: 152 Acre-feet (At top of dam)

Height: 12.5 feet

Potential Loss of Life:

Heavily used road (Main Street) traverses dam crest. Failure of dam could possibly cause loss of life.

Potential Economic Loss:

Dam failure would cause severe damage to Main Street which is a heavily used county road (Route 535).

Therefore, Brainerd Lake Dam is classified as "Small" size and "Significant" hazard potential.

d. Ownership

Brainerd Lake Dam is owned by the County of Middlesex, P. O. Box 1110, New Brunswick, New Jersey 08903.

e. Purpose of Dam

The purpose of the dam is the impoundment of a lake used for recreation.

# f. Design and Construction History

Brainerd Lake Dam reportedly was originally constructed in 1840. It is also believed to have been rebuilt in 1910. No plans for the construction of the dam could be obtained for this report.

# g. Normal Operation Procedures

The dam and appurtenances are operated by the Township of Cranbury, whereas maintenance is performed by the County of Middlesex, Department of Roads and Bridges. There is no fixed schedule of maintenance; repairs are made as the need arises.

The outlet works is used to drain the lake for maintenance purposes and during times of high water level to attenuate flooding conditions.

10.8 square miles

87.2

77.6

84.0 (Estimated)

# 1.3 Pertinent Data

C

Drainage Area

Spillway crest

Maximum tailwater

Stream bed at centerline of dam

	_	•	
<b>)</b> .	Discharge at Damsite		
	Maximum flood at damsite	Unknown	
	Outlet works at pool elevation	121 c.f.s.	
	Spillway capacity at top of dam	524 c.f.s.	
: <b>.</b>	Elevation (N.G.V.D.)		
	Top of dam	90.1	
	Maximum pool-design surcharge	91.8	
	Recreation pool	88.0	

#### d. Reservoir

Length of maximum pool 4200 feet (Estimated)
Length of recreation pool 3800 feet (Scaled)

# e. Storage (Acre-feet)

Recreation pool 60 acre-feet
Design surcharge 318 acre-feet
Top of dam 152 acre-feet

# f. Reservoir Surface (Acres)

Top of dam 132 acres (Estimated)

Maximum pool 222 acres (Estimated)

Recreation pool 22 acres

Spillway crest 20 acres

#### g. Dam

Type Earthfill road embankment

Length 382 feet

Height 12.5 feet

Sideslopes

Embankments - Upstream Vertical

- Downstream

3 horiz. to 1 vert.

Zoning Unknown
Impervious core Unknown
Cutoff Unknown
Grout curtain Unknown

h. Diversion and Regulating Tunnel N.A.

# i. Spillway

Type
Length of weir
Crest elevation
Gates
Approach channel
Discharge channel

Uncontrolled concrete weir 32 feet 87.2 N.A. N.A. Stone and brick arch

culvert through dam

j. Regulating Outlet

42-inch diameter lift gate

# SECTION 2: ENGINEERING DATA

# 2.1 Design

No calculations, reports or plans pertaining to the design of the dam are available.

## 2.2 Construction

No data or reports pertaining to the construction of the dam are available.

# 2.3 Operation

No records of operation of the lake or dam and no inspection reports subsequent to construction are available.

# 2.4 Evaluation

#### a. Availability

No engineering information is available for the subject dam.

## b. Adequacy

Available engineering data pertaining to Brainerd Lake Dam are not adequate to be of significant assistance to the performance of a Phase I evaluation. A list of absent information is included in paragraph 7.1.b.

#### c. Validity

The validity of engineering data cannot be assessed due to the absence of data.

#### SECTION 3: VISUAL INSPECTION

# 3.1 Findings

#### a. General

The inspection of Brainerd Lake Dam took place on November 12, 1979 by members of the staff of Storch Engineers. A copy of the visual inspection check list is contained in Appendix 1. The following procedures were employed for the inspection:

- 1) The embankment of the dam, appurtenant structures and adjacent areas were examined.
- 2) The embankment and appurtenant structures were measured and key elevations determined by a surveyor's level.
- 3) The embankment and appurtenant structures and adjacent areas were photographed.
- 4) Depths of water were measured at various locations in the lake.

#### b. Dam

The dam embankment forms the base for a roadway, paved with bituminous pavement, which appeared to be in good condition. A few trees were observed along both sides of the roadway. There were no signs of settlement, seepage, or sloughing of the embankment.

A stone masonry wall with a concrete cap forms the upstream face of the dam embankment. The concrete cap is in generally good condition, however the stone wall shows signs of deterioration, with some stones and mortar dislodged. A concrete patch approximately 15 feet long was observed near the south end of the wall.

The downstream slope of the embankment, north of the discharge channel was grass-covered, uniformly graded and in good condition. The downstream face south of the discharge channel consists of a concrete wall which forms the wingwall for the discharge channel and a stone masonry wall running parallel to the dam. The stone masonry wall was in generally satisfactory condition with evidence of numerous patches in the grout. Minor erosion was observed at the junction of the downstream face of the dam and spillway discharge culvert.

# c. Spillway

The spillway structure consists of a concrete, horseshoe-shaped wall located at the upstream end of the arch culvert. Although the surfaces were obscured by overflow, the structure appeared generally sound. The crest appeared to be partially spalled. The apron forming the bottom of the small stilling basin encircled by the spillway weir was obscured by tailwater and not observed.

Two planks in the walkway were partially rotted although the remainder of the walkway and railing was in generally good condition.

The brick surface of the culvert appeared to be in generally satisfactory condition with some patching and loose bricks noted on the north side near the upstream end. A crack, or separation, between the brickwork and stonework at the downstream end was noted.

#### d. Outlet Works

The outlet works consist of a 42-inch diameter lift gate located in the spillway structure. The upstream side of the gate was submerged and the downstream side was obstructed by the discharge over the spillway. Reportedly, during dry periods signs of leakage are visible from the downstream side.

There was no operating wheel on the outlet mechanism and therefore the gate was not tested at the time of inspection.

#### e. Downstream Channel

Flow through the arch culvert discharges into a natural stream lined by a concrete wall on the south side, and stone rubble walls and riprap on the north side. The condition of the concrete was good, although the wall was leaning into the stream approximately 6 inches.

#### f. Reservoir Area

Brainerd Lake is long and narrow averaging 250 feet in width and 3800 feet in length. Shores of the lake are grassed on the west portion and generally wooded along the east, or upstream portion of the lake. Soundings at various locations in the lake indicated little accumulation of sediment.

#### SECTION 4: OPERATIONAL PROCEDURES

# 4.1 Procedures

The water level in Brainerd Lake is regulated naturally by discharge over the spillway. Reportedly each year the outlet works are opened to permit a drawdown of approximately 4 feet to allow maintenance of lakefront properties. Also, the outlet is opened at times of intense storms in order to attenuate flood water level.

The time required to draw down the lake is estimated to be approximately 8 hours.

# 4.2 Maintenance of the Dam

There is no program of regular inspection and maintenance of the dam and appurtenant structures. Maintenance is performed on an "as needed" basis.

# 4.3 Maintenance of Operating Facilities

Maintenance of operating facilities is performed on an "as needed" basis.

# 4.4 Description of Warning System

Reportedly, no formal warning system is in use at the present time.

# 4.5 Evaluation of Operational Adequacy

The operation of the dam has been unsatisfactory to the extent that the dam was reportedly overtopped by 18 inches in the summer of 1975.

Maintenance documentation is poor but the overall condition of the dam indicates that significant attention has been directed toward the upkeep of the dam. However, areas of maintenance that have not been adequately performed are:

- 1) Trees on embankment not removed.
- 2) Stone masonry wall on upstream face of dam not completely repaired.
- 3) Some deterioration of brick arch culvert not completely repaired.
- 4) Two partially rotted planks in walkway not replaced.

#### SECTION 5: HYDRAULIC/HYDROLOGIC

#### 5.1 Evaluation of Features

# a. Design Data

The quantity of storm water runoff that the spillway should be able to pass without an overtopping of the dam is based on the size and hazard classification of the dam. This runoff, called the Spillway Design Flood (SDF), is described in terms of frequency or probable maximum flood (PMF) depending on the extent of the dam's size and potential hazard. According to the "Recommended Guidelines for Safety Inspection of Dams," published by the U.S. Army Corps of Engineers, the SDF for Brainerd Lake Dam falls in a range of 100-year frequency to 1/2 PMF. In this case, the low end of the range, 100-year frequency, is chosen since the factors used to select size classification are on the low side of their respective ranges.

The SDF hydrograph for Brainerd Lake was computed by use of the HEC-1-DB computer program using the SCS Method. Hydrologic computations and computer output are contained in Appendix 4. The calculated SDF peak inflow for Brainerd Lake Dam is 3222 c.f.s.

Discharge capacity for the spillway was computed by considering free discharge over the spillway weir. Hydraulic computations are contained in Appendix 4. The spillway discharge with lake level equal to the top of dam was computed to be 524 c.f.s.

The SDF was routed through the dam by the use of the HEC-1-DB computer program using the modified Puls method. In routing the SDF, it was found that the dam would be

overtopped by a depth of 1.7 feet above the crest. Accordingly, the subject spillway is assessed as being inadequate in accordance with criteria developed by the U.S. Army Corps of Engineers.

#### b. Experience Data

Reportedly, Brainerd Lake Dam was overtopped by 18 inches in 1975. Apparently no significant damage was sustained by the dam or the downstream area at that time.

#### c. Visual Observation

No evidence was found at the time of inspection that would indicate that the dam had been overtopped.

# d. Overtopping Potential

As indicated in paragraph 5.1.a, a storm of magnitude equivalent to the SDF would cause overtopping of the dam by a height of 1.7 above the top of the dam. The spillway is capable of passing approximately 16 percent of the SDF.

#### SECTION 6: STRUCTURAL STABILITY

# 6.1 Evaluation of Structural Stability

#### a. Visual Observations

The embankment appeared, at the time of inspection, to be outwardly stable. No significant indications of distress were observed nor was settlement, seepage or sloughing noted.

#### b. Generalized Soil Description

The generalized soils description of the dam site consists of recent alluvium, composed of stratified materials deposited by streams, overlying a discontinuous mantle of stratified, alluvial material deposited during the Quaternary period, known as the Pensauken Formation. The Quaternary deposits consist of sand, silty sand and sandy silt. The underlying formations are consolidated Cretaceous sediments known as Magothy and Raritan Formations.

# c. Design and Construction Data

Analyses of structural stability and construction data for the embankment and spillway structure are not available.

# d. Operating Records

No operating records are available for the dam. The water level of Brainerd Lake is not monitored.

# e. Post Construction Changes

No records of any post construction changes are available.

# f. Seismic Stability

Brainerd Lake Dam is located in Seismic Zone 1 as defined in "Recommended Guideline for Safety Inspection of Dams," which is a zone of very low seismic activity. Experience indicates that dams in Seismic Zone 1 will have adequate stability under seismic loading conditions if they have adequate stability under static loading conditions. Brainerd Lake Dam appeared to be outwardly stable under static loading conditions at the time of inspection.

## SECTION 7: ASSESSMENT AND RECOMMENDATIONS

#### 7.1 Dam Assessment

a. Based on hydraulic and hydrologic analyses outlined in Section 5 and Appendix 4, the spillway of Brainerd Lake Dam is considered inadequate. The spillway is not able to pass the SDF designated for the dam without an overtopping of the dam.

The dam appeared to be outwardly stable at the time of inspection. However, sufficient data is not available to allow a complete assessment of the present structural condition of the dam and appurtenances.

# b. Adequacy of Information

Information sources for this study include 1) field inspection,
2) USGS quadrangle sheet, 3) aerial photography from Middlesex
County, and 4) consultation with maintenance and operations
personnel from Middlesex County and Cranbury Township.

The information obtained is sufficient to allow a Phase I assessment as outlined in "Recommended Guidelines for Safety Inspection of Dams."

Some data not available are as follows:

- 1) Stream and lake gaging records.
- 2) Description of dam embankment structures and materials.
- 3) Hydraulic and structural design reports.
- 4) Construction and as-built drawings.
- 5) Maintenance documentation.
- 6) Inspection reports.

#### c. Necessity for Additional Data/Evaluation

Although engineering data pertaining to Brainerd Lake Dam is not available, additional data are not considered imperative for this Phase I evaluation.

#### 7.2 Recommendations

#### a. Remedial Measures

Based on hydraulic and hydrologic analyses outlined in paragraph 5.1.a, the spillway is considered to be inadequate. Therefore, it is recommended that a professional engineer experienced in the design and construction of dams be engaged in the near future to perform more accurate hydraulic and hydrologic analyses. Based on the findings of these analyses, the need for and type of remedial measures should be determined and then implemented.

The owner should, in the near future, develop an emergency action plan together with an effective warning system outlining actions to be taken by the operator to minimize downstream effects of an emergency at the dam.

In addition, it is recommended that the following remedial measures be implemented by the owner in the near future.

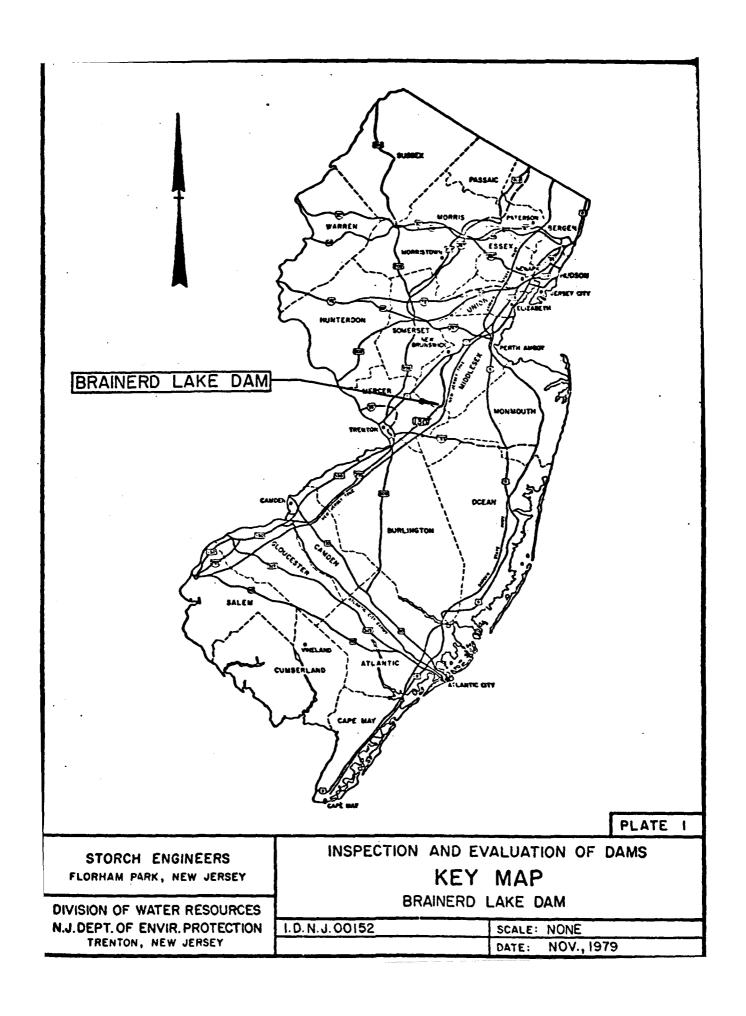
- With the lake drawn down, the masonry wall on the upstream side of dam should be thoroughly inspected and repaired.
- 2) The spillway structure and discharge culvert should be thoroughly inspected and repaired with the lake drawn down. Special attention should be given to the possibility of leakage in the spillway structure

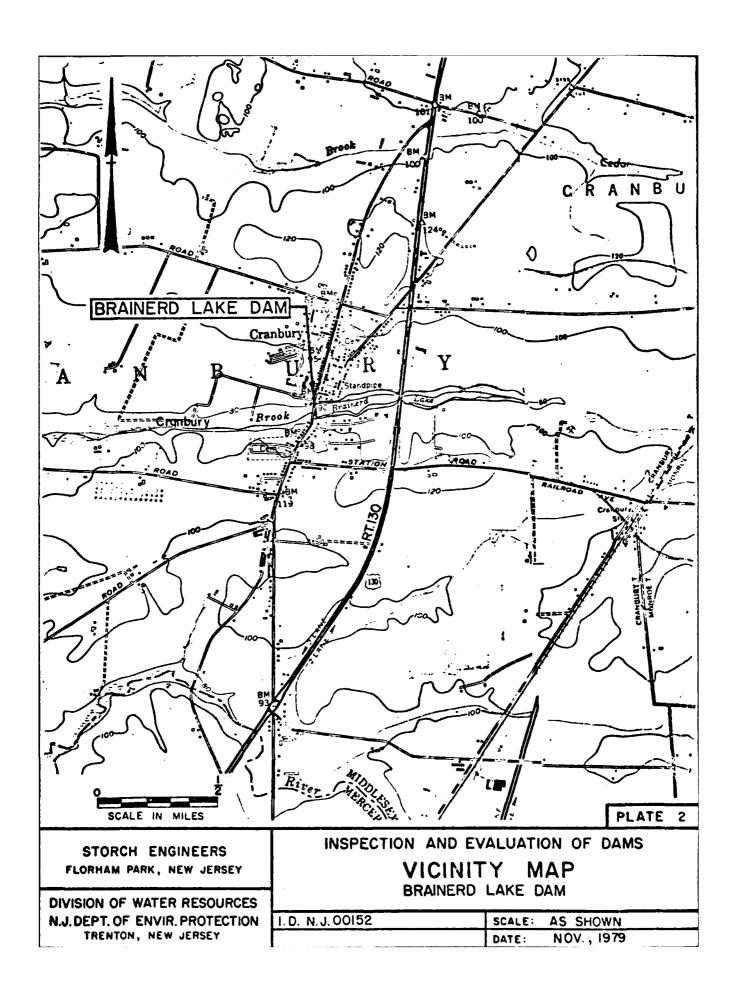
around the outlet works. Also, special attention should be given to the crack at the downstream end of the discharge culvert.

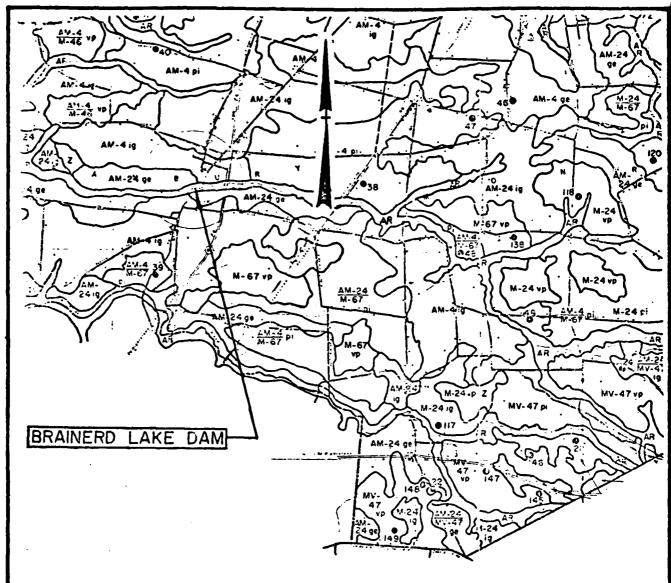
- 3) Trees on the embankment should be removed.
- 4) The partially rotted planks on the walkway should be replaced.

#### b. Maintenance

In the near future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to insure the safety of the dam. **PLATES** 







#### Legend

AR Recent alluvium composed of stratified materials

deposited by streams.

AM-24 Sand, silty sand and sandy silt deposited during

the Quanterary period. (Pensauken Formation).

NOTE: Information taken from Rutgers University Soil Survey

of New Jersey, Report No. 10, Middlesex County, and

Geological Map of New Jersey prepared by Lewis and Kummel.

PLATE 3

STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY

INSPECTION AND EVALUATION OF DAMS

SOIL MAP

BRAINERD LAKE DAM

DIVISION OF WATER RESOURCES
N.J. DEPT. OF ENVIR. PROTECTION
TRENTON, NEW JERSEY

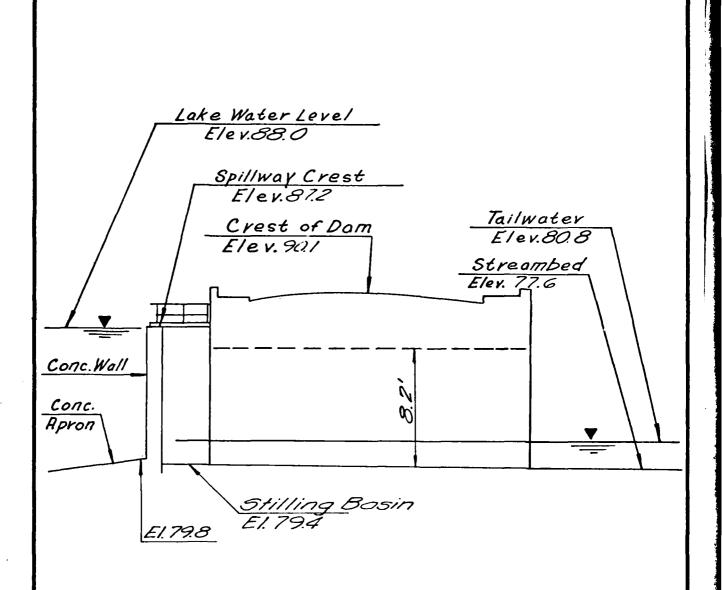
I.D. NJ 00152

SCALE: NONE

DATE: NOV., 1979

BRAINERD Overall Len Upstream Face (Masonory Noll) Note: Information taken from field inspection November 12,1979 1

ERD LAKE 11 Length of Dam = 382' Outlet Control Walkway Spillway 34'± Brick Arch Culvert Sidewolks Paved Road 20' MosonRy Wall PLATE 4 Downstreom DIVISION OF WATER RESOURCES Chonnel STORCH ENGINEERS N.J. DEPT. OF ENVIR. PROTECTION FLORHAM PARK, NEW JERSEY TRENTON, NEW JERSEY INSPECTION AND EVALUATION OF DAMS GENERAL PLAN BRAINERD LAKE DAM I.D. N.J. 00152 SCALE: NO TO SCALE DATE: DEC. 1979



#### Notes:

- 1. Information taken from field inspection November 12, 1979.
- 2. Elevations based on Benchmark provided by the Town of Cronbury.

PLATE 5

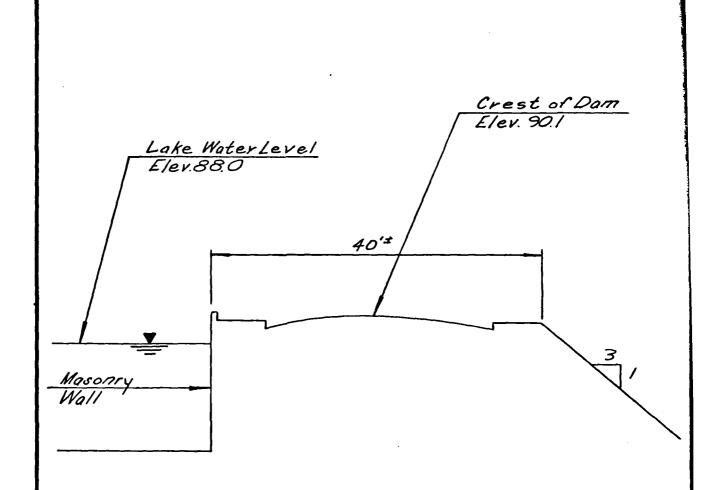
STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY

DIVISION OF WATER RESOURCES
N.J. DEPT. OF ENVIR. PROTECTION
TRENTON, NEW JERSEY

INSPECTION AND EVALUATION OF DAMS
SPILLWAY SECTION

BRAINERD LAKE DAM

I.D. N.J. 00152 SCALE: NOT TO SCALE
DATE: DEC. 1979



Notes:

1. Information taken from plan
by John E. Studer September,
1949 and field inspection
November 19, 1979
2. Elevations based on Benchmark
provided by Township of Cranbury.

PLATE 6

STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY

DIVISION OF WATER RESOURCES
N.J. DEPT. OF ENVIR. PROTECTION
TRENTON, NEW JERSEY

INSPECTION AND EVALUATION OF DAMS

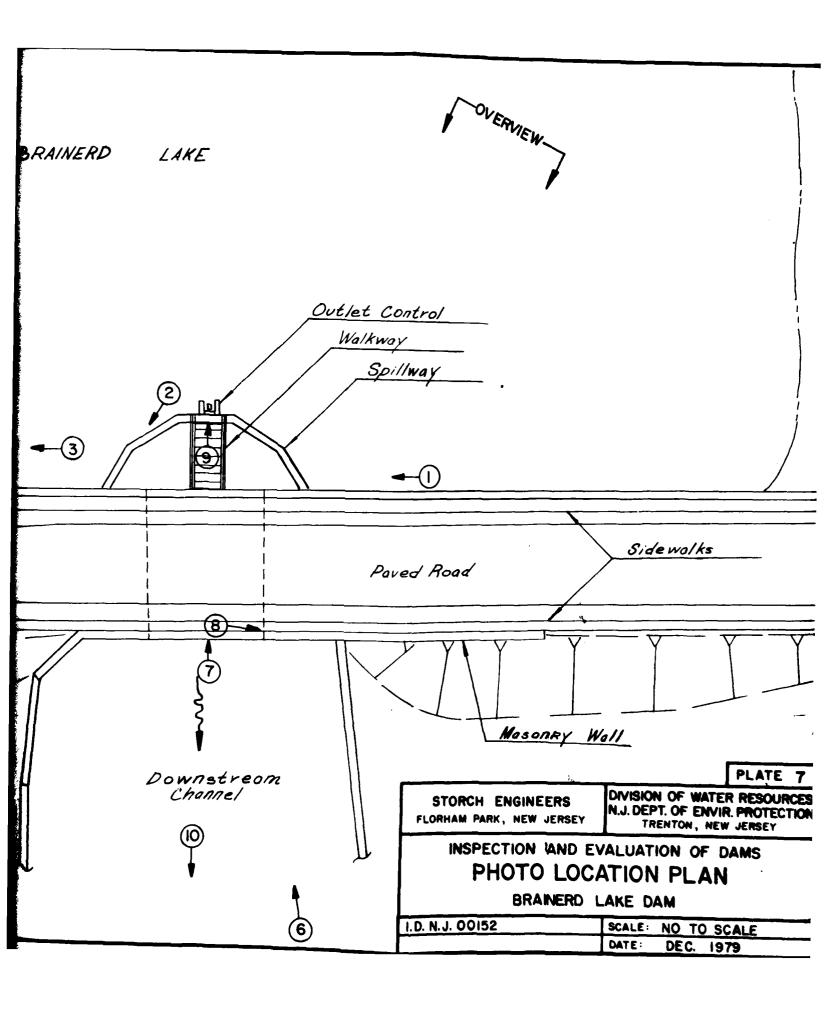
DAM SECTION BRAINERD LAKE DAM

I.D.N.J.00152

SCALE: NOT TO SCALE

DATE: JAN. 1980

BRAINERD Upstream Face (Masonory Woll) **→**3 Note: Information taken from field inspection November 12, 1979.



### APPENDIX 1

Check List - Visual Inspection Check List - Engineering Data Check List Visual Inspection Phase I

Name of Dam Brainerd Lake Dam	County Middlesex	State New Jersey : Coordinators NJDEP
Date(s) Inspection 11/12/79	Weather P-Cloudy	Temperature 45°F
Pool Elevation at Time of Inspection 88.0 M.S.L.	lon 88.0 M.S.L.	Tailwater at Time of Inspection 80.8 M.S.L.
Inspection Personnel:		
John Gribbin	Alan Volle	
Ronald Lai	Thomas Miller	
Richard McDermott		-
	J. Gribbin	Recorder

### EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
GENERAL	Paved roadway on crest of embankment in generally satisfactory condition. Downstream face uniformly graded and grass covered. A few trees were observed along both sides of the roadway.	
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Junction between spillway and embankment generally sound with minor erosion.	•
ANY NOTICEABLE SEEPAGE	None observed.	
STAFF GAGE AND RECORDER	None observed.	
DRAINS	No toe drains observed. Storm water drains discharging into lake appeared to be in generally satisfactory condition. Weep holes in stone masonry wall at spilłway observed - condition could not be determined.	
		•

## EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed.	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None observed.	
SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES	No sloughing observed. Minor erosion observed at junction of downstream face of dam and spillway discharge culvert.	
WERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	Vertical: Generally level. Horizontal: Straight	
UPSTREAM FACE	Stone masonry wall appeared generally stable with some deterioration including dislodged stones and mortar.	Upstream face is formed by stone masonry wall with concrete cap. Recommend repair of wall with lake drawn down.

# OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SURFACES IN: OUTLET CONDUIT	Not observed.	
INTAKE STRUCTURE	Not observed. (Submerged)	Recommend inspection with lake drawn down.
OUTLET STRUCTURE	Not observed - obscured by discharge over spillway.	
OUTLET CHANNEL	Same as spillway discharge channel.	
GATE AND GATE HOUSING	Gate not observed. Operating mechanism appeared to be in satisfactory condition, not operated at time of inspection.	

# SPILLWAY

REMARKS OR RECOMMENDATIONS			Discharge channel consists of brick arch culvert through dam.		
OBSERVATIONS	Spillway structure appeared generally sound - surfaces were obscured by discharge. Concrete crest was partially spalled.	N.A.	Brick surface of culvert appeared to be generally satisfactory with some patching and loose bricks noted on the north side near the upstream end. A crack, or separation, between the brickwork and stonework at the downstream end was noted.	The apron forming the bottom of a small stilling basin encircled by the spillway weir was obscured by tail water and not observed.	
VISUAL EXAMINATION OF	WEIR	APPROACH CHANNEL	DISCHARGE CHANNEL	APRON	·

# INSTRUMENTATION

VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	•
OBSERVATION WELLS	None	
WEIRS	None	·
DIEZAMETEDE		
TECOME ERS	None	
0.11.10		
X .	N.A.	

### RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Shores of lake are grassed along the west portion of the lake and wooded along the east portion. Slopes are approximately 6 horiz. to 1 vert.	
SEDIMENTATION	Soundings at various locations in the lake indicated the presence of little sediment accumulation.	
STRUCTURES ALONG BANKS	Several dwellings are located along the west portion of the lake. The Route 130 bridge is located on the lake approximately 1800 feet from its west end.	
·		

# DOWNS:TREAM CHANNEL

REMARKS OR RECOMMENDATIONS				
OBSERVATIONS	The downstream channel is a natural stream with walled sides in the vicinity of the dam. No significant obstructions were observed.	Bank slopes vary from 10 horiz. to 1 vert. to 2 horiz. to 1 vert. Banks are generally wooded.	Two dwellings are located in the vicinity of the dam and lie above its crest. One shed is located approximately 1300 feet downstream.	
VISUAL EXAMINATION OF	CCNDITION (OBSTRUCTIONS, DEBRIS, ETC.)	SLOPES	STRUCTURES ALONG BANKS	

### CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

		Not Available Not Available Not Available	DAM - PLAN  SECTIONS  SPILLWAY - PLAN  SECTIONS  DETAILS  OPERATING EQUIPMENT PLANS & DETAILS  OUTLETS - PLAN  DETAILS  CONSTRAINTS  DISCHARGE RATINGS  HYDRAULIC/HYDROLOGIC DATA
		Not Available .	RAINFALL/RESERVOIR RECORDS
		Not Available	HYDRAULIC/HYDROLOGIC DATA
	•	Not Available	HYDRAULIC/HYDROLOGIC DATA
	: .		DISCHARGE RATINGS
	-		CONSTRAINTS
			DETAILS
		Not Available	OUTLETS - PLAN
		Not Available	OPERATING EQUIPMENT PLANS & DETAILS
	•		DETAILS .
			SECTIONS
		Not Available	SPILLWAY - PLAN
		·	SECTIONS
•		Not Available	

REMARKS Not Available Not Available GEOLOGY REPORTS DESIGN REPORTS

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
DAM STABILLITY
SEEPAGE STUDIES

MATERIALS INVESTIGATIONS
BORING RECORDS
LABORATORY
FIELD

POST-CONSTRUCTION SURVEYS OF DAM Not Available

BORROW SOURCES

Not Available

Not Available Not Available Not Available Not Available POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS MONITORING SYSTEMS HIGH POOL RECORDS MODIFICATIONS

PRIOR ACCIDENTS OR FAILURE OF DAM Not Available DESCRIPTION REPORTS

MAINTENANCE OPERATION RECORDS

Not Available

APPENDIX 2

Photographs

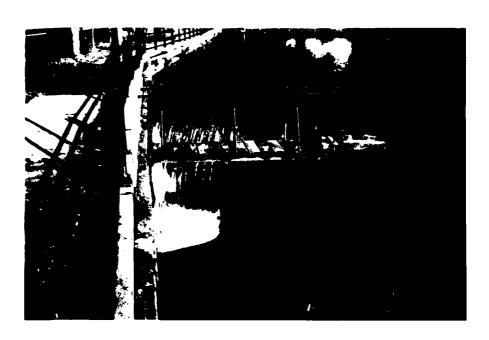


PHOTO 1 SPILLWAY

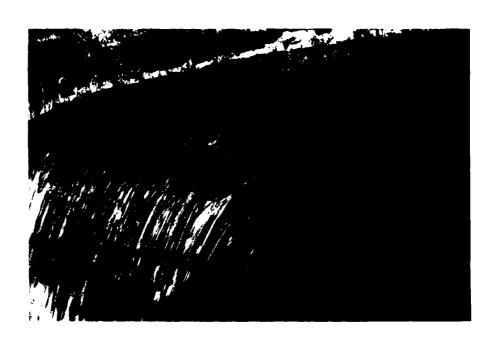


PHOTO 2 SPILLWAY CREST

BRAINERD LAKE DAM 12 NOVEMBER 1979



PHOTO 3

UPSTREAM FACE OF DAM - LOOKING NORTH



PHOTO 4

UPSTREAM FACE OF DAM - LOOKING SOUTH

BRAINERD LAKE DAM 12 NOVEMBER 1979



PHOTO 5

12 NOVEMBER 1979

DOWNSTREAM FACE OF DAM



PHOTO 6

PHOTO 6

DOWNSTREAM VIEW OF SPILLWAY AND SPILLWAY DISCHARGE

BRAINERD LAKE DAM



PHOTO 7
SPILLWAY DISCHARGE CULVERT



PHOTO 8

CRACK AT DOWNSTREAM END OF DISCHARGE CULVERT

BRAINERD LAKE DAM 12 NOVEMBER 1979

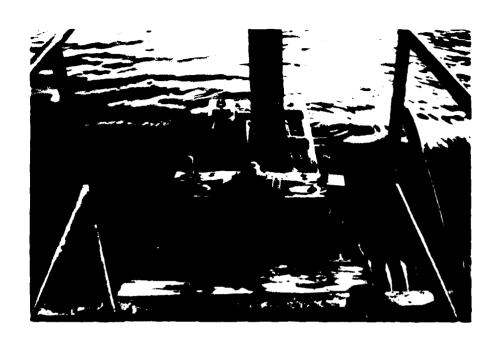


PHOTO 9
OUTLET WORKS OPERATING MECHANISM



PHOTO 10

DOWNSTREAM CHANNEL

BRAINERD LAKE DAM 12 NOVEMBER 1979

### APPENDIX 3

Engineering Data

### CHECK LIST HYDROLOGIC AND HYDRAULIC DATA

#### ENGINEERING DATA

DRAINAGE A	REA CHARACTERISTICS: Mostly undeveloped fields
ELEVATION	TOP NORMAL POOL (STORAGE CAPACITY): 88.0 (60 acre -feet)
ELEVATION	TOP FLOOD CONTROL POOL (STORAGE CAPACITY): N.A.
ELEVATION	MAXIMUM DESIGN POOL: 91.8
ELEVATION	TOP DAM: 90.1
SPILLWAY C	REST: Uncontrolled concrete weir
a.	Elevation87.2
	Type Broad crested
	Width 1.2 feet
	Length 32 feet
	Location Spillover Upstream side of dam
	Number and Type of Gates N. A.
	KS: 42-inch gate on upstream side of spillway wall
a.	Type Sluice with lift gate
<b>b.</b>	Location Upstream end of spillway structure
c.	Entrance inverts 79.4
d.	Exit inverts 79.4
e.	Emergency draindown facilities: Open gate
HYDROMETEO	ROLOGICAL GAGES: None
a.	TypeN.A
<b>ს.</b>	LocationN.A.
с.	RecordsN.A.
	N-DAMAGING DISCHARGE:
(1.240	stand onual to too of dam) 524 c f s

### APPENDIX 4

Hydraulic/Hydrologic Computations

Made By STO Date 1/28/30

Chkd By RL Date 2/7/80

### HYDROLOGY

HYDROLOGIC ANALYSIS - RUNOFF HYDROGRAPH WILL

BE DEVELOPED BY HEC-I-DB USING SCS TRIANGULAR

HYDROGRAPH WITH CURVILINEAR TRANSFORMATION.

DEAMAGE AREA = 10.8 SQUARE MILES.

INFILTRATION DATA - MOSTLY UNDEVELOPED

USE: INITAL INFILTRATION = 1.5 INCHES / HOUR

### TIME OF CONCENTRATION

BY SCS; TR-SS CHART ON OVERLAND FLOW

OVERLAND FLOW: 4000' @ 3.3% V= 1.3 FPS

CHANNEL FLOW = 43500' @ 0.16%; V- 1 FPS

TC = [4000 + 43500] 1/3600

TC = 0.8 HOURS (OVERLAND) + 12.1 HOURS (CHANNEL)

TC = 12.9 HOURS

Made By STO Date 1/28/80

Chkd By RL Date 2/7/80

OVERLAND TIME OF CONCENTRATION - BY KERBY

Ref: "HANDBOOK OF APPUED HYDROLOGY"

BY CHOW

Tc214 = 2/3 Ln/15

Tre-overland time of concentration ( min)

L=length of overland flow (ft)
n. Roughness coefficient (n=0.4)

5 = slope (f+/f+)

Tc 2.14 = 2/3 4000 (0.4)/V.033

TC = 58 MINUTES = 0.96 HOURS ~ 1.0 HOUR

TOTAL TC: 1.0 HOURS (OVERAND) + 12.1 HOURS (CHANNEZ)

TL: 13.1 HOURS

TIME OF CONCENTRATION - BY CALIFORNIA CULVERTS PRACTICE
Ref: "DESIGN OF SMALL DAMS" Pg.71

 $T_C = \left(\frac{11.9 \text{ L}^3}{4}\right)^{0.385}$ 

Tc = time of concentration (hours)

L = longth of watercourse (miks)

H = elevation difference (feet)

 $T_c = \left[\frac{11.9 (8.2)^3}{70}\right]^{0.385}$ 

L= 43500' = 8.2 MILES H= 70'

Tc = 5.74 HOURS

Sheet 3 of 9 \_\_Made By <u>STD</u> Date 1 /28/80

Chkd By 16 Date 3/3/80

TIME OF CONCENTRATION - BY SNYDER IA: PG 135
"INTRODUCTION TO HYDROLOGY" VIESSMAN et al.

te = Ct (6 Lca) 0.3

Where: ty = LAG TIME (HOURS)

Ct = COEFFICIENT REPRESENTING VARIATIONS OF

WATERSHED SLOPES & SURFACES (ANE = 2.0)

L= LENGTH OF MAIN CHANNEL FROM OUTLET

TO DIVIDE (9.0 MILES)

LCQ = LENGTH ALONG MAIN CHANNEL TO A

POINT OPPOSITE THE WATERSHED

CENTROID (4.3 MILES)

tt= 2.0 (9.0 × 4.3) 0.3 LAG TIME = 6.0 HOURS

FOR COMPUTER INPUT & USE To = 11.0 HOURS

LAG TIME = 0.6 × 11.0

LAG TIME = 6.6 HOURS

Sheet\_\_\_\_\_\_ of \_\_\_\_\_9

Made By <u>STO</u> Date 1/28/30

Chkd By 15 Date 3/3/80

### 24- HOUR RAWFALL DISTRIBUTION (AT 15 MIN. INTERVAL

		,	<del></del> -					
INTERVAL	HOUR-MIN	RAWFALL (INCIES)	wter/al	HOUR- MIN.	RAWFALL (INCHES)	INTERIAL	HOUR -MIN.	RAINFAL (INCHES)
1	0 - 15	.020	33	- 15	.037	65	15	.100
2	. 30	.020	34	30	.037	66	30	.100
3	45	.020	35	45	.037	67	45	,100
4	1.0	.020	36	9-0	.037	68	17-0	.100
5	15	.020	37	15	ر30،	69	15	.084
6	30	.021	38	30	.037	10	30	.083
7	45	.021	39	45	,037	71	45	.083
8	2- 0	.021	40	10-0	.037	12	18-0	.083
9	15	.021	41	15	.038	73	15	.038
10	30	.021	42	30	,038	74	30	.038
lı lı	45	.021	43	45	.038	15	45	,038
12	3-0	,021	44	11 - 0	,038	16	19- 0	.038
13	15	.021	45	- 15	.038	n	15	.037
14	30	.021	46	-30	.०३८	18	30	.037
15	45	.021	47	-45	.038	79	45	.037
16	4 -0	,021	48	12 -0	.038	80	20-0	.037
เก	15	,021	49	-15	.083	81	15	.021
18	30	.021	50	30	.083	82	30	150.
19	45	.021	51	45	.083	83	45	1051
20	5-0	,021	52	13 -0	.083	84	21-0	150,
21	15	,021	53	15	.083	85	ıs	150.
22	30	.021	54	30	.084	86	30	.021
23	45	1501	55	45	.084	87	45	150.
24	6-0	1021	56	14 -0	.084	88	22-0	1021
25	15	.021	51	15	. 220	89	15	150.
26	30	.021	58	30	.220	90	30	.021
27	45	.७21	59	45	. 230	91	45	1021
28	7-0	.021	60	15-0	.230	92	23.0	,071
29	15	021	61	15	. ,270	93	15	<b>,</b> ०घ
30	30	150,	62	30	.770	94	30	م٥٥,
31	. 45	.021	63	45	1.680	95	45	, 050
32	8-0	.021	64	16.0	.280	96	24.0	. 070

Project BRAINERD LAKE DAM

Made By STO Date 1/23/30

Sheet \_\_\_\_5\_\_ of \_\_\_9\_

Chkd By RL Date 2/7/80

### LAKE STORAGE VOLUME

WATER SURFACE ELEVATION SURFACE AREA (ACRES) 79.8 0 88 22 653 100

HEC- 1- DB COMPUTER PROGRAM WILL GENERATE STORAGE CAPACITY FROM SURFACE AREAS & ELEVATIONS.

INFORMATION OBTAINED FROM USGS QUADRANGLE AND SOUNDINGS TAKEN DURING FIELD INSPECTION.

Sheet <u>6</u> of <u>9</u>

Made By STD Date 1/21/80

Chkd By RL Date 2/ 7/80

### HYDRAULICS

THE SPILLWAY AT BRAINERD LAKE IS A CONCRETE,
HORSESHOE-SHAPED, FREE OVERFLOW WEIR, THE SPILLWAY IS
AT ELEVATION 87.2; WITH AN EFFECTIVE LENGTH OF 32'
(34' TOTAL - 2' OBSTRUCTED BY OUTLET WORKS MECHANISM)

DISCHARGE WILL BE TABULATED USING THE FORMULA;

Q= CLH<sup>3/2</sup> WHERE: Q= discharge over spillway

C= discharge coefficient

L= effective length of spillway

H+ total head on spillway

DISCHARGE VALUES IN THE FOLLOWING TABULATION DO NOT INCLUDE OVERTOPPING OF 356' (382' TOTAL - 26' OF DAM CREST NOT OVERTOPAED, DOWNSTREAM OF SPILLWAY) OF DAM CREST AT ELEVATION 90.1, AS THIS WILL BE COMPUTED BY THE HEC-1-DB COMPUTER PROGRAM

VALUES FOR THE DISCHARGE COEFFICIENT, "C" WHERE

TAKEN FROM THE "HANDBOOK OF HYDRAULICS"

-BY KING & BRATER.

Project BRAINERD LAKE DAM

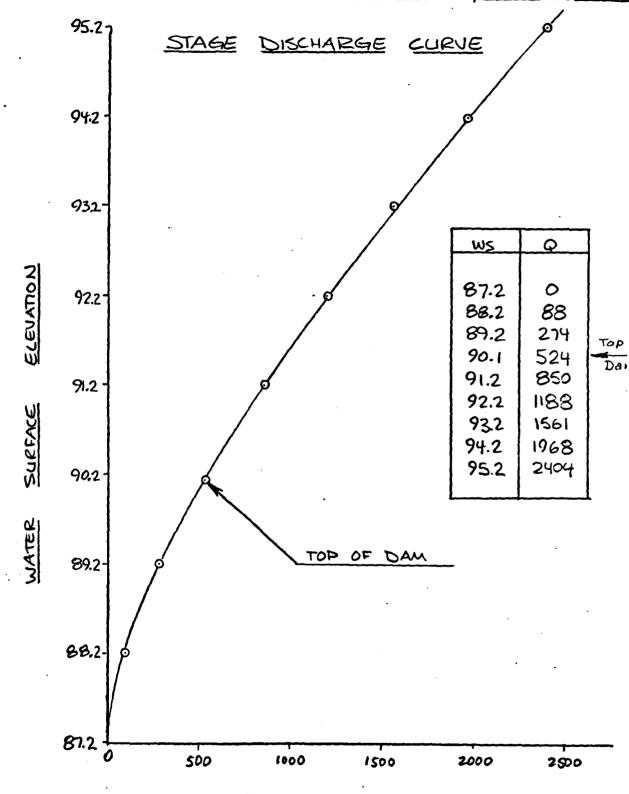
Made By STO Date 1/24/80 Child By RL Date 2/7/80

DISCHARGE TABULATION STAGE

WATER SURFACE ELEVATION	HEAD (FT)	"c"	DISCHARGE (CFS)
87.2	0	-	0
88.2	1	2.75	88
89.2	2	3.03	274
90.1	2.9	332	524
91.2	4	3,32	850
92.2	5	3.32	1188
93.2	6	3.32	1561
94.2	ז	3.32	1968
95.2	8	3,32	2404
96.2	9	3.32	2868

Sheet \_ \_ & \_ of \_ \_ C Made By <u>\$70</u> Date <u>1/24/3</u>

Chkd By RL Date 2/7/8



DISCHARGE (CFS)

Project BRAINERD LAKE DAM Made By STO Date 1/29/80

Chkd By RL Date 2/7/80

## <u>OUTLET</u> WOPKS CAPACITY

THE OUTLET WORKS AT BRAINERD LAKE CONSIST OF 3.5' ROUND SLIDE GATE LOCATED WITHIN THE SPILLWAY SECTION, ASSUME DRAWDOWN BY LIFTING GATE. DRAWDOWN DISCHARGE WILL BE MADE TREATING GATE AS A SUBMERGED ORIFICE USING THE EQUATION, Q= CAVZgh

A= 9.62 SF

C=0.6 h = 2.6 (ave.)

 $Q = (0.6)(9.6) \sqrt{2}(32.2)(2.6)$ 

Q= 75 CFS (AUERAGE)

Q AT POOL ELEVATION 88.0 = 121 CFS

DRAWDOWN - STORAGE AT SPILLWAY DRAWDOWN DISCHARGE - NORMAL INFLOW

> (43560 SF/Ac) = 44 AC-FT 75 CFS - (1 CFS/SM × 10.8 SM) (3600 SEC/HR)

= 8.3 Hours

HEC-1-DB COMPUTATIONS

					90.	0	.03	80	52		200						96.2 2868			
	ю				\$0°		.03	80	۲ د د د د د د د د د د د د د د د د د د	2 M 3 C	0.0						95.2			
					.02	20	03	• 03	\$25	٥ ا	0.021		0.15				94 • 2 1968			
6 R A R				ERD LA	• 02	90	.03	• 03	25	- K	0.00		1.5		DAM	α	93.02 1561			
TY PRO E DAM ROUTT	-		4	ERAIN	• 02	200	0.3	. n 3	æ 0		0.023	.02			THRU		92.2			
DAM SAFE INERD LAK FAR STORM	, ,		ROGRAPH TO		• 02	90	000	.03	(C)	0 10	0.021	• 02			DISCHARGE	-	91.8 850			
NATIONAL PRA 100 Y	-		4	LOW HYDR	- 02	000	) ()	03	α o	. c	000	• 02			ROUTE	<b>+</b>	90°1			356
	15	-	;	10.8	20.	0.0	0.15	.03	×0.	40 P 40 C 40 C	000	.02		2 • 0			• 1-	: 653 100		1.5
	0	-	LAKE	8	20.	• ·	20.	.03	0	<u> </u>	0.000	0.2	. ,	6.05 0.05 0.05	٩.		23 83 83	0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	•	2 • 63
	200	D=4e	40		•	0°0	200	.03	0 8	200		70.	l	-1.0	<b>→</b>	•	87.2	2		9

DATER 80/03/13.

ROM E

00 20 00		N N N N N	NATIO 10 I I I I I I I I I I I I I I I I I I I	NAL DAM BRAINERD O YEAR S JOB SPEC	NATIONAL DAM SAFETY PROGRAM BRAINFRD LAKE DAM 100 YEAR STORM ROUTING UOB SPECIFICATION 100		IPLT IPRT NSTAN	IPRT	NSTAN	
			30PER 5	2	LKOPI	18 40 E				
			1LT1-PL	N ANALYS	ES TO BE	MULTI-PLAN ANALYSES TO BE PERFORMED	<b>Q</b>			
2	RTIOS= 1.00		4	- KZ	10-1-14	-01-				

LOCAL ISTAGE ISAME INAME ISNOW RATIO 0.000 INFLCW HYDROGRAPH TO BRAINERD LAKE SUB-AREA RUNDEF COMPUTATION JPLT P DATA DAS PATTERN HYDROGRAPH DATA TRSDA TRSPC 10.80 0.00 ITAPE IECON SHAP 0.00 TCOMP 78 1 AREA-TUME IMYDG

ALSHX 0.00 CNSTL 15 RTIOR = 2.00 UNIT HYDPOGRAPH DATA RECESSION DATA ERAIN STRKS A COORDINATE OF -1.00 10= 1.00 1.00 STRTG= OLTKR 0.00 STRKS 0.00 LROPI WELLING TO SOLUTION OF THE SOL 00000000000

200000000

	D.DA HR.MN	PERIOD	RAIN	EXCS	LOSS	COMP G
	.01 .15 1.01 .30	- 1	02	0.00	.02 .02	10.
	1.01 1.66	- 2 3 4 5	02	0.00	.02	9.
	1.01	5	• 65	0.00	.02	i ř.
	1.01 1.45 1.01 2.00 1.01 2.15 1.01 2.45 1.01 3.00	7	.02 .02	0.00	.02	7. 6.
	01 2.15	8	.05	0.00	.02	6.
	1.01 2.10 1.01 2.45	11	•02	0.00	.02 .02 .02	5. 5.
	1.01 3.00 1.01 3.15	12 13	.02		•02	5.
	1.01 3.30	14 15	.02	0.00	02	
		16	.02	0.00	• 02 • 02 • 02	•
	1.01 4.15 1.01 4.30 1.01 4.45 1.01 5.15 1.01 5.45 1.01 6.00	17		0.00 -	:02	3:
	1.01 4.45 1.01 5.00	1901 221 223 24	•02	0.00	•02	3. 3.
	1.01 5.15 1.01 5.30	- 21	.02	0.00	•02	3·
	1.01 5.45 1.01 6.00	23	.02	0.00	•02	2.
	1.01 6.13	25	.05	0.00	•05	2.
	1.01 6.30	25 26 27		0.00	022000000000000000000000000000000000000	2.
	1.01 6.45 1.01 7.00 1.01 7.15	2 n 2 y	-02	0.00	• 02	2. 1.
	7.30	30	02 02		02	1.
	1.21 8.00	333 335 35	• 05	Ğ • Ö Ö	.02	1.
-	1.01 8.15	33 34	.04	0.00	04	1:
	1.01 E.45 1.01 5.00	35 36	.04 .04	0.00	• 04 • 04	1:
	1.01 9.15 1.01 9.30	37	04	0.00	04	i.
	1.01 9.45	- 18	• C 4	0.00	- 04	1:
	.01 10.00 1.01 10.15	40	.04 .04	0.00	• 0 4 • 0 4	1.
	1.01 10.30 1.01 10.45	42	04 04	0.00	- C4	i:
	1.01 11.00	44	.04	0.00	.04	1.
i,	01 11.15 01 11.30	45 46	0.4	0.00	• 04 • 04	0.
	1.01 11.45	47	.04	0.00	• 04 • 04	0.
	12.00 12.15 1.01 12.30 1.01 12.45 1.01 13.00 1.01 13.30 1.01 13.45	49	0 8 0 8	0.00	•0∂	0.
	12.45	50 51	• •08	.01	.08	0.
1.01	13.00	52 53	.08 .08	•05	.04 .04	1.
1.01	13.15 13.30 13.45 14.00	^ 54 55	.0A	• 05	.04	3 6
1.0		56		.05 .05 .05 .05	04	9 15
	1.01 14.30	57 58	. 25	•10	.04	23.
į	.01 14.45 .01 15.00	5 9 6 0	• 53	•19 •19	.04	34. 49.
:	.01 15.00 .01 15.15 .01 15.30	61	· • • • • • • • • • • • • • • • • • • •	•23 •73	:04	70.
	.01 15.45 .01 16.00	62 63 64	.02 .22 .23 .27 .76 1.68	1.64	.04	149. 206.
:	.01 16.15 .01 16.30	65	- 10	•24 •06	04	279. 371.
	1.01 16.45	67	.10	•06	.04	371. 471.
	1.01 17.00 1.01 17.15	6 d 6 9	•10 •08	•06 •05	.04	583. 706.
	17.30	70	- 08 08	.05	.04	938.
	18.60	72	-08	0.5	0.4	1140.
- ;	• 01 15 • 30	7.3	04	·ğğ	04	1567.
	1.01 19.00	76	•04 •04	.00	.04	1698. 1895.
	1.01 19.15	77	- 04	0.00	- 04	2096. 2289. 2463. 2627.
	1.01 19.45	79	ěğá	0.00	Ŏ	2463.
;	01 20.15	51	02	0.00	.02	2773.
_	1.01 20.30 1.01 20.45	- 82 63	•05	0.00	.05	2998.
;	21.00	84	.02	0.00	• 02	2892. 2998. 3082. 3145. 3194. 3215.
. :	.ci 21.30	86	05	0.00	: 05	3194.
	22.00	8 7 8 0	.05	0.00	•02	3222.
	1.01 22.15 1.01 22.30	9n	- 02	0.00	- 05	3218.
;	01 22 45	ģ į	.ŏž	0.00	.02	3169. 3169.
	23.15	23	.02	0.00	.02	3051.
	23.45	95	.05	0.00	.05	2977• 289 <b>4•</b>
	01 17 0505 17 05505 17 0505 17 0505	090123456789012345678901234567890 10001234567890 10001234567890	10000000000000000000000000000000000000		0.00	580. 788. 788. 1389. 11427. 11599. 120
	1.02 .30	98	0.00·	0.00	0.00-	··· 5615.

MC.D/	A HR.MN	PERIOD	RAIN	Excs	LOSS	COMP 0	
1.02 1.02 1.02	1:15	101 102 103	0.00	0.00 0.00 0.00	0.00	2276. 2154. 2027.	
1.02 1.02 1.02 1.02 1.02	2.00	103 104 105	0.00	0.00 0.00	0.00 0.00 0.00	1898. 1773.	
	2.30	106 107	0.00	0.00	0.00		-
1.02	3.15	108 109 110		0.00 0.00 0.00	0.00	1660. 1552. 1454. 1367. 1295.	
	3.45	110 111 112 113 114	0.00	0.00	0.00	1208.	
1.02	4.30	113 114 115		000000000000000000000000000000000000000		1135. 1066. 1004. 945. E90. 843. 797.	
1.02	5.00	115 116 117 1189 120 1212 1223 124	0.00	0.00	0.00	890. 843.	
1.02	5.45 5.45	118 119 120	0.00	0.00	0.00	757. 752. 708.	-
1.0	6.15	121 122	0.00	0.00	0.00	752. 708. 666. 628. 597.	
1.02	7.00	123 124 125	0.00	0.00	0.00 0.00	5°2. 5°7. 522.	
1.0	7.30	125 126 127 128 129	0.00	0.00	0.00	490	
1.02 1.02 1.02 1.02 1.02	2 8.15 2 8.30	128	0.00	0.00	0.00	20.000 20.000 20.6315.000 44316.3354.235.353.353.353.353.353.353.353.353.353	
1.0	8.45 9.00	130 131 132 133	0.00	0.00	0.00	363. 341.	
—— 1.02 1.02	9.10	134 135	0.00 0.00 0.00 0.00	0.00	0.00	303. 285.	
1.02 1.02 1.03	9.30 9.45 10.00 10.15	134 135 136 137 138				26F • 251 • 237 •	
1.02 1.02 1.02 1.02 1.02 1.02	100-050505050505050505050505050505050505	138 139 140		0.00	0.00	223. 210.	-
1.02	11.30	140 141 142 143	0.00	0.00	0.00	197. 185. 174.	
1.02	12.05050505050505050505050505050505050505	144	0.00	0.00	0.00	164.	
1.02	12.30	146	0.00	0.00	0.00	137	
1.02	13.00 13.15 13.30	148 149 150	0.00 0.00		0.00	155. 146. 137. 129. 172.	
1.02	13.45	151 152	0.00	0.00	0.00	100.	
1.02 1.02	14.30	153 154 155	0.00	0.00	0.00 0.00 0.00	102. 96. 90. 85.	
1.02	15.00	156 157	0.00	0.00	0.00	80. 75.	
1.02	15.15 15.30 15.45 16.00 16.15	159 160	0.00	0.00 0.00 0.00	0 • 0 0 0 • 0 0 0 • 0 0 0 • 0 0	67. 63.	
- 1.02	16.15	1455234567 R 9 0 1 2 3 4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.00 0.00 0.00 0.00	0.00	0.00	59• 56•	
1.02	16.30 16.45 17.00	164 165	0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.00 0.00	0 • 0 0 0 • 0 0 0 • 0 0 0 • 0 0	52. 49. 46.	
1.02	17.15 17.30 17.45	166 167 168	0.00	0.00		41:	-
1.02	10.15	169 170	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	39. 37. 35.	
1.02	19.00	171 172	0.00	0.00	0.00	33. 32.	
1.02	\$50505050505050505050505050505050505050	174 175	0.00	0.70 0.30 0.00	0.00	29. 27.	
1.02	20.00	176 177	0.00	0.00	0.00	26.	
1.02	20.45	179 180	0.00	0.00	0.00	21. 20.	
1:02 1:02	21.15	181 182	0.00	0.00	0.00	18. 17.	
1.02	22.00	163 164 185	0.00	0.00	0.00	15. 15.	
1.02	22.30	196 187	0.00	0.00	0.00	13. 12.	-
1.02	23.15	188 189 190	0.00	0.00	0.00	11:	
1.02	23.45	191 192	0.00	0.00	0.00	9.	
1.03	30	193 194 195	0.00	00000000000000000000000000000000000000	00000000000000000000000000000000000000	2553. 309. 2274. 2274. 2274. 116. 119. 111. 119. 111. 119. 111.	
1.03	1.00	136	0.00	0.00	0.00	7. 7. 6. 6.	
	\$0.50\$0505050505050505050505050505050505	117723456789012345678901234567890 1177277777788888888888999999999999999999		0.00 0.00 0.00	0.00	6. 5. 5.	
		SUP	7.20	4.27	2.93	119311. 3378.51	
			( 183.)	( 109.)(	74.)(	3378.51	7

HYDROGRAPH ROUTING  ROUTE DISCHARGE THRU DAH  ISTAG ICOMP IECON ITAPE UPLT JPRT INAME ISTAGE IAUTO  0.055 CLOSS AVG IRES ISAME 10PT IPMP LSTR  NSTPL LAG AMSKK 0.000 0.000 52.00 95.20 95.20  NSTPS NSTDL LAG AMSKK 0.000 0.000 188.00 1968.00 2.000  NSTPS NSTPS NSTDL LAG AMSKK 0.000 0.000 188.00 1968.00 2.000  IION 80.0 52. 653.  IION 80.0 60. 3240.  IION 60. 524.00 EXPU ELEVI COOL CAREA EXPL			NOTE TO SECOND		3222	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000 • • • • • • • • • • • • • • • • • •	10 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		- • • • • • • • • • • • • • • • • • • •	;			
STAG   ICOMP   IECON   ITAPE   JPRT   INAME   ISTAGE   IAUTO	•	•		•	•	:				:		•		
STAG   ICOMP   IECON   ITAPE   JPRT   INAME   ISTAGE   IAUTO		! !				HYDROGI	MAPH ROU	LING				• •		
ROUTING DATA  RO		:		ISTAG	1CO4P	TECON TECON	ITAPE	UDAR	L & Q	INAMI	ISTAGE	IAUTO		
NSTPS NSTDL LAG AMSKK 0.000 0.000 -88. ISPRAT 87.20 88.20 89.20 90.10 91.20 92.20 93.20 94.20 95.20 NREA = 0. 22. 653. 117 = 0. 60. 3240. 110N = 80. 88. 100. 100 0.00 0.00 0.00 0.00 0.000 0.00 0.00				CL255	AV6.00	IRES 1	ING DAT		- 0 - 0 - 0 - 1	:	LSTR	:		
87.20 88.20 89.20 90.10 91.20 92.20 93.20 94.20 95.20  NREA = 0.00 274.00 524.00 850.00 1188.00 1561.00 1968.00 2404.00  SITY = 0.00 60. 3240.  TION = 80.0 R8. 100.  EXPL  CAREA EXPL		; ; ; !	,	NSTPS	NSTDL	LAG	AMSKK 0.000			STORA-88.	ISPRAT'	* *	:	
NREA = 0. 22. 653. 524.00 850.00 1188.00 1561.00 1968.00 2404.00		87.20	88.20	<b>6</b> 0	9.20	90.1		91.20	92.20	•	3.20	94.20	95.20	96.20
0. 22. 653. 0. 60. 3240. 80. 88. 100. 87.2 SPYID COQU EXPU ELEVE COQU CAREA	FLOV	00.0	88.00-	27	00.	- 524.00	1	20.00	1188.00	1 50	1.00	1968.00		2868.00
80. 88. 100. COGU EXFU ELEVE COGU CAREA	FACE AREA =	•			653.									
	CAPACITY=	•	,		240.	:	!	:						
SPAID COOK COOK COOK COOK COOK CAREA	ELEVATION=	9			100.	-								
	,	1	875	ļ	1	ļ		EV. C0			70	:		

	MO.DA	HR.MN	END-0 PERIOD	F-PER I HOURS	OD HYDR		PH CRDINA	TES ST	ORAGE		STAGE	
	1.01	•30 •45	<u>1</u>	•25 •50 •75	<del></del> 1	9.	66 61 57		59. 58. 57.		87.9 87.9 87.8	
	1.01	1.00		- 1.00 - 1.25		ģ.	53 49		56. 55.		87.8 87.8	
	1.01	1.30	<b>6</b>	1.50		Ž:	46•		54. 53.		87.7 87.7	
	1.01	2.00	<u> </u>	2.00		6.	39. 36.		53. 52.		87.6 87.6	
	1.01	2.30	10	2.50		5.	34. 31.		51. 51.		87.6 87.6	
	1.01	3.00 3.15	11 12 13	3.00		5.	29 27		50.		87.5 87.5	
	1.01	3.30 3.45	14 15	3.50			25 23		49.		87.5	
	1.01	4.00	16	4 - 0 0		4:	21. 20.		49.		87.5 87.4 87.4	
	1.01 1.01	4.30	18 19	4.25 4.50 4.75		3. 3.	18. 17.		48.		87.4	
	1.01	5.00	20	5.00		3.	16.		48.		87.4 87.4 87.4	
	1.01	5.15 5.30	21 22 23	5.25 5.50 5.75		3.	13.		47:		87.4	
	1.01	5.45	24	6.00		5.	12.		47.		87.3 87.3	
	1.01	6.15	25 26	6.25		2.	11.		46.		87.3 87.3 87.3	
	1.01	6.45 7.00	27 28 29 30	6.75 7.00		Ş.	9		46.		67.3	
	1.01	7.15 7.30	30	7.25 7.50 7.75		1:	7:		46.		87.3 87.3 87.3	
	1.01	7.45 8.00	31 32 33	. 8.00		1:	7. 6.		46.		87.3 87.3	
	1.01	8.15	34	8.25 8.50 8.75		1:	5.		45.		87.3 87.3 87.3 87.3	*********
	1.01	8.45 9.00	35 36	9.00		1:	5. 4.		45.		# / A S	
	1.01	9.15	37 38	9.25 9.50 9.75		1:	**		45.	•	87.2 87.2 87.2	
	1.01	9.45 10.00	39 40	10.00		1:	3:		45.		87.2 87.2	
	1:01	10.30	41 42 43	10.25 10.50 10.75		1:	3.		45.		87 • 2 87 • 2 87 • 2 87 • 2 87 • 2 87 • 2	
	1.01	10.45	44			1:	3.		45.		87.2 87.2	
	1.01	11.15	45	11.25		٥.	2.		45.	•	87.2 87.2	
	1.01	11.15 11.30 11.45 12.00	47 48	11.25 11.50 11.75 12.00		0.	2.		45. 45.		87.2	
	1.01	12.15	49 50	12.50		0.	2.		45.		87.2	
	1.01	12.45	51 52	12.75 13.00 13.25 13.50		0.	i. 1.		44.		87.2 87.2	
	1.01	13.15	53 54	13.25		2.	i.		44.		87.2 87.2 87.2	
	1.01	13.45	55 56	13.75		6.	<u> </u>		45. 45.		87.2 87.2 87.2 87.3	
	1.01	14.15	57 58	14.25 14.50 14.75			3. 5.		45.		87.2	
	1.01	14.45	59 60	14.75 15.00		9	7. 10.		46.		87.3 87.3	
	1.01	- 15.15- 15.30	61	15.25 15.50		, Ó .	15.		47.		87.4 87.4	
	1.01	15.45	63	15.75	14	19.	30. 43.		51.		87.5 87.7	
	-1.01	- 16.15- 16.30	64 65 66	16.25	2	)6. 79.	60:		- 54. 58.		87.9	
	1.01	16.45	67	16.25 16.50 16.75 17.00	47	į	81. 120.		63. 69.		88.4	
	-1:01	17.15-	69	17.25	7	6.	216.		· 87.		88.9	
	1.01	17.45	71	17.75	98	19.	333.		110.		89.1	
	- 1:01	18.15		18.25	13	0.	481.		125		89.7	
	1:01	18.30 18.45	74 75	18.50 18.75	169	98.	589. 822.		159. 178.		90.2	
	1.01	19.00 19.15	76 77 ·	19.00 19.25	209	95. 96.	1082.		195. 212.		90.7 90.8	
	1.01	19.30 19.45	78 79	19.50 19.75	229 246	33.	1587. 1819.		227.		91.0 91.1	
	1.01	20.00	80 18	20.00	267	77.	2036		253. 265.		91.3	
	1.01	20.30	82 83	20.50	289	22.	2417. 2577.		275.		91.5	
	1.01	21.00	. 84	21.00	308	2.	2716.		293.		91.6	
•	1.01	21.30	86	21.50	319	4.	2936.		306.		91.7	
	1.01	22.00	88	22.00	322	ž	68207643. 68207643. 112237643. 12237643. 12237777666. 1235813577766. 1235813577766. 1235813577766. 1235813577766. 1235813577766. 12358135813577766. 123581358135777677677677677677677677677677677677677		314.		88899000000000000000000000000000000000	
	1.01	22.30	90	22.50	315	9	3144.		318.		91.8	
	1.01	23.00	92	23.00	312	Ž.	3152.		318		91.8 91.8	
=	1.01	23.30	94	23.50	291	77:	3098.		315.		91.8	
	1.05	0.00	96 96	24.00	580 583	6.	2991•		309.		91.8 91.8 91.7	
-	1.02	.30	97	24.50	271 261	2	2923. 2847.		305. 300.		91.7	
	1.02	1.00	100	24.75 25.00	250 239	57.	2760. 2667.		295. 290.		91.6	

	1.02 " 1.15	101	25.25	2276		2567.		284.	91.5	
	1.02 1.30 1.02 1.45	103	25.25 25.50 25.75	2154 2027		2461. 2349.		278. 271.	91.5 91.4	
	1.02 2.00 1.02 2.15	105	24 00	1898 1773	·	2232.		265. 258.	91.4 91.3	
	1.02 2.30 1.02 2.45	107	26.25 26.50 26.75	1660 1552	•	1992. 1877.		251. 244.	91.2 91.2	
	1.02 3.00 1.02 3.15	108		1367		1766. 1662.		237.	91.1 91.0	
	1.02 3.30 1.02 3.45	110	27.25 - 27.50 27.75	1285 1208		1563.		225. 220.	91.0 90.9	
	1.02 4.00	112	28.00	1135	•	1384.		214.	90.9	
	1.02 4.30	114	28.25 - 28.50 28.75	1004		1226.		204.	90.8 90.7	
	1.02 5.00 1.02 5.15 1.02 5.30	116 117 118	29.00 29.25 - 29.50 29.75		١.	1089.		196.	90.7	
	1.02 5.30 1.02 5.45	118 119	29.50	797 752	<b>'•</b>	971.		185. 185.	90.6 90.5	
· .	1.02 5.00	120		708	•	869. 823.		181.	90.5	
	1.02 6.30	122	30.25 30.50 30.75	666 628 592	•	779. 737.		178.	90.4	
	1.02 7.00	124	31.00	557	•	699.		172. 169.	90.4	
	1.02 7.15 1.02 7.30	126	31.25 - 31.50 31.75	522 490	١.	662. 628.		166.	90.3 90.3	
	1.02 7.45 1.02 8.00	128		461	١ ـ	597. 569.		160.	90 • 2 90 • 2	
	1.02 - 8.15 1.02 8.30	129	32.50	386	•	544. 524.		155. 152.	90.1 90.1	
	1.02 3.45 1.02 9.00	131	32.75	363 341 322	. •	512. 499.		149.	90.1 90.0	
	1.02 - 9.15 1.02 - 9.30	133	33.25 " 33.50	303	•	485. 471.		142. 139.	90.0 89.9	
	1.02 9.45 1.02 10.00	135 136	322-705 322-705 333-705 333-705 333-705	265 268	•	456. 440.		135. 132.	89.9 89.8	
	1.02 10.30	138	34 • 25 34 • 5 0 34 • 75 35 • 00	251 237	:	423.		128. 125.	89.7 89.7	
	1.02 10.45 1.02 11.00	139	34.75 35.00	223		390. 373.		121. 118.	89.6 89.6	
	1.02 11.15 1.02 11.30	141	35.25 35.50	191		356. 338.		115.	89.5 89.4	
	1.02 11.45	1 4 3	15 76	174	•	321. 305.		108.	89.4 89.3	
	1.02 12.00 1.02 12.15 1.02 12.30	145 146	36.25	155	•	298. 273.		102.	89.3 89.2	
	1.02 12.45 1.02 13.00	147 148	36.25 36.50 36.75 37.00	13 129	' <b>.</b>	262. 251.		97. 95.	89.1 89.1	
	1.02 13.15 1.02 13.30	149	37.25 37.50 37.75	iž	•	229		92. 90.	89.0	
	1.02 13.45	151	37.75 38.00	108		219.		Ŕ7. 85.	88.9 88.8	
	1.02 14.15	153	38.25 38.50	196 90	•	197. 197.		83. 81.	88.8	
	1.02 14.30 1.02 14.45	155	38.75	8.5	•	176.		79.	88.7	
· <del>-</del>	1.02 15.00 1.02 15.15 1.02 15.30	- 156 - 157	39.00 39.25 39.50	<u>6</u> 0		166. 156.		77. 75.	88.6 88.6	
	1.02 15.45	157 158 159	39.75	7 1 6 3	<b>7</b> •	147. 138.		74. 72.	88.5	
	1.02 16.15	160 161	40.00	53	•	129.		71. 70.	88.4 88.4	
	1.02 16.30 1.02 16.45	163	40.75 40.75 41.00	52	•	112. 105.		68. 67.	88.3 88.3	
	1.02 17.00 1.02 17.15	165	41.25	49		97. 91.		66. 65.	86.3 88.2	
	1.02 17.30 1.02 17.45	167	91.75	4.7		86. 83.		64. 63.	88 • 2 88 • 1	
<del></del> .	1.02 19.00 1.02 18.15	169	42.25	3		- 80. 77.		63. 62.	88 · 1	****
	1.02 18.30 1.02 18.45	170	42.25 42.50 42.75	3 5 3 3	•	74. 71.		61. 60.	88.0 98.0	
J	1.02 19.00	172 173 174	43.C0	33		68.		59. 59. 58.	84.0 87.9	
	19.000.000.000.000.000.000.000.000.000.0	174	43.50	2000	•	59. 59. 54. 51.		58. 57.	8477777666655555544487777766665555554487777777777	
	1.02 20.00	176	44.00	26		56°		2/.	87.8 87.8	
	1.02 20.30	178	44.50	21		51.		56 • 55 •	87.8	
	1.02 21.00	180	45.00	- ž	•	6		55. 54. 54. 53. 53.	87.7	
	1.02 21.30	182	45.50	į		12.		53.	Ř7.7	
<b>.</b>	1.02 22.00	184	46.00		•	38		žž.	87.6	
	1.02 22.30	175 1776 1776 1778 178 1891 181 183 184 185 185	46.50	14 12 12 13 14 15 16 17		96420 4420 43353222222222223		52. 52. 51. 51.	87.6	
	1.02 23.00	188	47.00	1	•	31.		51.	87.5	
	1.05 53.30	190	47.50	10	•	27.		50. 50. 50.	87.5	
	1.03 23.45	191 192	47.75 48.00	Ġ		26. 24.		49.	87.5 87.5	
	1.03 .15	192 193 194 195 196	98.25 48.50	7		- 23. 22.	•	49.	87.5 87.4	
	1.03 .45	195 196	48.75	3		20.		48.	87.4 87.4	
	1.03 .45 1.03 1.00 1.03 1.15 1.03 1.30	148	4333444445566667770505050505050505050505050505050		•	1 8 • 1 7 • 1 6 •		48. 48.	67.4 67.4 87.4 87.4	
	1.03 1.45 1.03 2.00	177	49.75 50.00	•	•	16.		48.	87.4 87.4	
<u></u>										

## SUMMARY OF DAM SAFETY ANALYSIS

The second secon

	TIME FAILURE HOURS	00.0	
90-10 152-0 524-	TIME OF MAX OUTFLOW HOURS	22.75	
109	DURATION OVER TOP HOURS	14.25	
SPILLWAY CREST	MAXIMUM OUTFLOW CFS	3156.	
INITIAL VALUE 88.00 60.	MAYIMUM STORAGE ACHFT	318.	
INITIAL 88	MAXIMUM DEPTH OVER DAM	1.71	
ELEVATION STORAGE OUTFLOW	R MANA WAR WAR SANGE WAS S	91.81	
•	8 8 4 1 0 8 7 1 0 8 7 1 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.00	

APPENDIX 5

Bibliography

 "Recommended Guidelines for Safety Inspection of Dams," Department of the Army, Office of the Chief of Engineers, Washington, D.C. 20314. 

- Design of Small Dams, Second Edition, United States Department of the Interior, Bureau of Reclamation, United States Government Printing Office, Washington, D.C., 1973.
- 3. Holman, William W. and Jumikis, Alfreds R., Engineering Soil

  Survey of New Jersey, Report No. 10, Middlesex County, Rutgers
  University, New Brunswick, N.J., 1953.
- 4. "Geologic Map of New Jersey," prepared by J. Volney Lewis and Henry B. Kummel, dated 1910 1912.
- Chow, Ven Te., Ed., <u>Handbook of Applied Hydrology</u>, McGraw-Hill Book Company, 1964.
- Herr, Lester A., <u>Hydraulic Charts for the Selection of Highway Culverts</u>,
   U.S. Department of Transportation, Federal Highway Administration, 1965.
- 7. <u>Safety of Small Dams</u>, Proceedings of the Engineering Foundation Conference, American Society of Civil Engineers, 1974.
- 8. King, Horace Williams and Brater, Ernest F., Handbook of Hydraulics, Fifth Edition, McGraw-Hill Book Company, 1963.
- 9. <u>Urban Hydrology for Small Watersheds, Technical Release No. 55, Engineering Division, Soil Conservation Service, U.S. Department of Agriculture, nuary 1975.</u>
- Viessman, Warren Jr., et al, <u>Introduction to Hydrology</u>, Second Edition, IEP, 1977.